Hypersonic Shock-Wave/Turbulent-Boundary-Layer **Interaction Flows**

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Abstract

HIS paper uses a two-dimensional/axisymmetric Navier-Stokes code to study the accuracy of the two-equation $k-\epsilon$ turbulence model¹ when compared with the hypersonic shockwave/boundary-layer interaction data base.2 Two modifications of the standard k- ϵ model are also investigated. The first is the new two-layer $k-\epsilon$ model developed by Rodi³ that has had good success for separated flows at low speeds. The second is a modification developed to account for compressibility effects following the work of Rubesin⁴ and Vuong and Coakley.⁵ These three models are evaluated by comparison with the data. The relative merits of the modifications are discussed.

Contents

Seven two-dimensional and axisymmetric experimental investigations were chosen for the current turbulence model evaluation process. These investigations include all four hypersonic studies recommended by Settles and Dobson² plus a recommended supersonic compression corner case, an additional axisymmetric cylinder-flare study, and a recent impinging shock study described in the full paper. For all of the test cases, either the flare, corner, or incident shock angles were varied to obtain flowfields with and without separation. Solutions were obtained using the three turbulence models described previously for 21 test cases. Only a few representative results will be shown here. Details of the turbulence models and computations including a mesh resolution study are given in the full paper.

Comparison of the computations and experiment for three selected test cases are shown in Figs. 1-3. The test geometry for all three cases is an axisymmetric cylinder flare. An attached flow at Mach 7.1 is shown on Fig. 1, and two separated cases at Mach 7.1 and 9.2 are shown on Figs. 2 and 3, respectively. In all cases, the data and computations are normalized by the same number for each test flow, namely, the average experimental value ahead of the interaction. For each test case, solutions with the three turbulence models are shown. Rather than discussing the individual test cases, several general observations will be made that are valid for most or all of the comparisions (including the 18 additional test cases not shown here due to space limitations).

The results obtained using the standard $k - \epsilon$ model underpredict the separation size and overpredict the skin friction and heat transfer near reattachment for the separated flow cases by substantial amounts. It performs similarly in the

Two-laver model - G - G - G - G adverse pressure gradient regions for attached flow cases. The Received May 10, 1991; presented as Paper 91-1760 at the AIAA 22nd Fluid Dynamics, Plasma Dynamics, and Lasers Conference, Honolulu, HI, June 24-26, 1991; synoptic received Aug. 7, 1991; accepted for publication Aug. 20, 1991. Full paper available from AIAA Library, 555 W. 57th St., New York, NY 10019. Copyright ©

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1991 by the American Institute of Aeronautics and Astronautics, Inc. No copyright is asserted in the United States under Title 17, U.S. Code. The U.S. Government has a royalty-free license to exercise all compressible model is in all cases an improvement or at least equal in performance to the standard $k-\epsilon$ model. The compressibility modifications increase separation zone size and decrease skin friction and heat transfer at reattachment and in

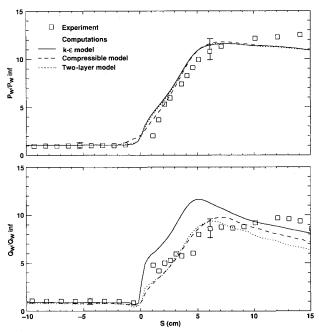


Fig. 1 Comparisons of surface pressure and heat transfer distributions; M = 7.1, 20-deg cylinder-flare flow.

Experiment

k-€ model Compressible m

Computations

Fig. 2 Comparisons of surface pressure and heat transfer distributions; M = 7.1, 35-deg cylinder-flare flow.

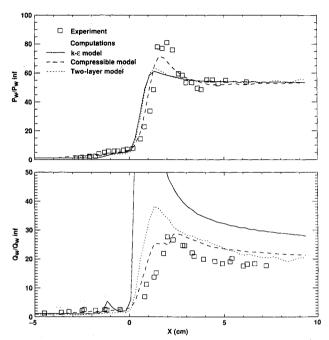


Fig. 3 Comparisons of surface pressure and heat transfer distributions; M = 9.2, 40-deg cylinder-flare flow.

adverse pressure gradient regions, thus giving better agreement with experiment.

The original intent of the two-layer model was to save computer time by allowing a more coarse mesh to be used.³ In the present hypersonic flow computations, this did not prove to be the case. The mesh requirements for this model are almost identical to those for the standard model. The computed results using this model did increase the predicted separation zone size and lowered the skin friction and heat transfer at reattachment, similar to the compressible model. However, in regions of zero and low-pressure gradient the computed

skin friction and heat transfer tended to underpredict the data. Other than this defect, the results are also better than or equal to the results using the standard model.

Solutions of the Reynolds-averaged Navier-Stokes equations using three turbulence models, including a model modified to account for compressibility effects, have been compared with several hypersonic shock-wave/turbulent-boundary-layer interaction test flows. The data available for comparison included surface pressure, skin friction, heat transfer, and the length of the flow separation zones. No single model accurately predicted all of the test cases; however, both the modified compressible model and the two-layer model showed substantial improvement over the standard $k-\epsilon$ model and could be used to predict unknown shock-wave/boundary-layer interaction flows with reasonable confidence. Considering the experimental errors present in the data (several experimenters do not even try to estimate their errors) and the ever-present computational errors due to numerical approximations and smoothing, the new compressible turbulence model described here seems adequate to solve these types of flowfields. Further improvements in turbulence modeling await a more complete data base that includes detailed fluctuating flow velocity, density, and temperature measurements.

References

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